### Комбинированное влияние уровня поступления питательных веществ и механических свойств тканей на рост доброкачественной опухоли



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### Growth-limiting factor #1: diffusional limitation of nutrient supply

#### Tumor spheroid – 3D model of tumor in vitro

# Experimental growth curves



Horman S. R. //Special Topics in Drug Discovery. – 2016. – p. 73.

Hardelauf H. et al. //Lab on a Chip. – 2011. – Vol. 11. – №. 3. – pp. 419-428.

### Mechanisms to overcome starvation



*Nature reviews cancer*, *3*(6), 401-410. (2003)

Vassilevski Y. et al. Personalized Computational Hemodynamics. – Academic Press, 2020.

### Growth-limiting factor #2: stress-induced growth inhibition

1000 1000 Free 0.5% 800 0.7% 800 -0.8% 0.8%(IIII) -1.0% Diameter (µm) 0.9% 600 600 1.0% Diameter 400 400 200 200 0 30 50 20 40 30 40 10 Time (days) Time (days)

Constant agarose concentration

Helmlinger G. et al. //Nature biotechnology. – 1997. – T. 15. – №. 8. – C. 778-783.

Gel release on 30<sup>th</sup> day

# Why model tumor growth with account of solid stress?













Seano G. et al. //Nature biomedical engineering. – 2019. – T. 3. – №. 3. – C. 230-245.

# Main model assumptions

- Spherically-symmetrical growth
- Non-invasive tumor
- Avascular tumor
- Biphasic tissue (porous solid matrix immersed in fluid)
- Solid stress is isotropic
- Densities of two phases are equal and constant

solid phase: 
$$\frac{\partial c}{\partial t} = \overbrace{F(c,g,\sigma)}^{\text{production}/} - \frac{1}{r^2} \frac{\partial (I_c cr^2)}{\partial r},$$
  
production/  
destruction  
destruction/  
destruction/  
 $\frac{\partial f}{\partial t} = -F(c,g,\sigma) - \frac{1}{r^2} \frac{\partial (I_f cr^2)}{\partial r},$ 

- Tissue is fully saturated:  $c + f = 1 \Rightarrow I_c c = -I_f f$
- External body forces are negligible
- Fluid flow is slow
- Solid phase permeability is homogeneous (but varied)

Darcy's

$$f(I_f - I_c) = -\frac{K}{\mu}$$

Porous media theory:





viscosity

gradient

## Full model

$$\begin{array}{ll} \text{tumor cells:} & \overbrace{\partial n}{\partial t} = \overbrace{Bn \cdot \Theta_p(g) \cdot \Theta_\sigma(\sigma)}^{\text{proliferation}} - Mn \cdot \Theta_d(g)}^{\text{convection}} - \overbrace{\frac{1}{r^2} \frac{\partial(I_c n r^2)}{\partial r}}^{\text{convection}}, \\ \text{normal cells:} & \overbrace{\partial h}{\partial t} = \overbrace{-\frac{1}{r^2} \frac{\partial(I_c h r^2)}{\partial r}}^{\text{convection}}, \\ \text{glucose:} & \overbrace{\partial g}{\partial t} = \overbrace{Ph[1-g]}^{\text{inflow}} + \overbrace{\frac{D_g}{r^2} \frac{\partial^2(g r^2)}{\partial r^2}}^{\text{consumption by proliferating cells}} \\ - Q_g n \cdot \{[1-\Theta_p(g)] \cdot \Theta_\sigma(\sigma) + [1-\Theta_\sigma(\sigma)]\} \cdot [1-\Theta_d(g)], \\ \hline - Q_q n \cdot \{[1-\Theta_p(g)] \cdot \Theta_\sigma(\sigma) + [1-\Theta_\sigma(\sigma)]\} \cdot [1-\Theta_d(g)], \\ \hline ecells \text{ velocity:} & I_c = -\frac{K}{\mu} \frac{\partial \sigma}{\partial r}, \\ \text{solid stress:} & \sigma \equiv \sigma(c) = \begin{cases} 0, \ c \leq c_s, \\ k \frac{[c-c_0] \cdot [c-c_s]^2}{[c_0-c_s]^2}, \ c_s < c < c_0, \end{cases} \\ \hline variation \text{ of } P: \\ 0.7*10^{-6} - 1.8*10^{-4} \text{ s}^{-1} \\ \text{Variation of } K/\mu: \\ 10^{-10} - 10^{-6} \text{ cm}^2/(\text{mmHgs}) \end{cases} \end{cases}$$

### Dependence of solid stress on cell fraction



# Infinite hydraulic conductivity limit $(K/\mu \rightarrow \infty)$

$$c = c_0$$

$$f = 1 - c_0$$

$$I_c = \frac{K \partial \sigma}{\mu \partial r}$$

tumor cells: 
$$\frac{\partial n}{\partial t} = \underbrace{Bn \cdot \Theta_p(g)}_{\text{convection}} - \underbrace{Mn \cdot \Theta_d(g)}_{\text{convection}} - \underbrace{\frac{1}{r^2} \frac{\partial(I_c n r^2)}{\partial r}}_{\frac{1}{r^2} \frac{\partial(I_c n r^2)}{\partial r}},$$
  
normal cells: 
$$\frac{\partial h}{\partial t} = -\underbrace{\frac{1}{r^2} \frac{\partial(I_c h r^2)}{\partial r}}_{\frac{1}{r^2} \frac{\partial^2(g r^2)}{\partial r^2}} - \underbrace{\frac{\text{consumption by proliferating and quiescent cells}}_{\frac{1}{r^2} \frac{\partial(I_c r^2)}{\partial r}} = \underbrace{\frac{1}{c_0} [Bn \cdot \Theta_p(g) - Mn \cdot \Theta_d(g)]}_{\frac{\Theta_p(g)}{\frac{1}{r^2} \frac{\partial(I_c r^2)}{\partial r}} = \frac{1}{c_0} [Bn \cdot \Theta_p(g) - Mn \cdot \Theta_d(g)], \qquad \underbrace{\Theta_p(g) = [1 + \tanh(\epsilon \{g - g_p\})]/2, \\ \Theta_d(g) = [1 + \tanh(\epsilon \{g_d - g_p\})]/2. \end{aligned}$$

#### Estimation of growth curves at $K/\mu \rightarrow \infty$



# Growth curves and comparison with numerical simulations



#### Intermediate hydraulic conductivity (K/µ=0.3)



#### Intermediate hydraulic conductivity (K/µ=0.3)



# Intermediate hydraulic conductivity (K/μ=0.3): fluid-filled core under high nutrient inflow



# Low hydraulic conductivity (K/ $\mu$ =0.03): crucial condition for giant benign tumors



# Very low hydraulic conductivity (K/ $\mu$ =0.003): stress-induced restriction and explosive acceleration



### Discussion

#### **Results:**

- Simple continuous model of benign tumor growth in normal tissue was presented.
   Nutrient supply and biomechanical interactions were accounted for.
- In the limit of infinite tissue hydraulic conductivity accurate tumor growth curves were obtained semi-analytically. Such limit is applicable for K/μ > 10<sup>-8</sup> cm<sup>2</sup>/(mmHg·s).
- Sufficiently low hydraulic conductivity and high nutrient supply level led to giant long-growing tumors.
   Lowest values of tissue hydraulic conductivity and high nutrient supply level yielded explosive tumor growth before reaching plateau.

Most crucial model drawback: neglect of circumferential stress.

#### Future work: optimization of tumor treatments,

associated with the delivery of drugs via intravenous injections.

# Thank you for your attention!

**Results are published:** 

Kuznetsov M.

Combined Influence of Nutrient Supply Level and Tissue Mechanical Properties on Benign Tumor Growth as Revealed by Mathematical Modeling // Mathematics. – 2021. – T. 9. – №. 18. – C. 2213.

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