



Validation of Finite-Volume Methods for Clot Formation Modelling

**Kirill Terekhov¹, Anass Bouchnita²,
Vitaly Volpert³, Yuri Vassilevski^{1,4,5}**

¹Marchuk Institute of Numerical Mathematics of the Russian Academy of Sciences

²Ecole Centrale Casablanca

³Institut Camille-Jordan, University of Lyon 1

⁴Sechenov University

⁵Moscow Institute of Physics and Technology

BIOMATH, 2 November 2020



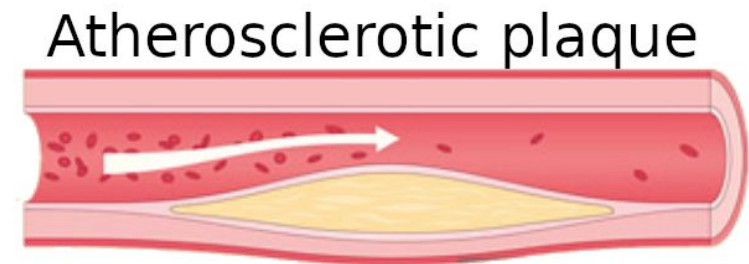
Problem

actuality and complexity



Problem:

- Construction of **three-dimensional** model of blood flow and coagulation, clot formation after damage of blood vessel

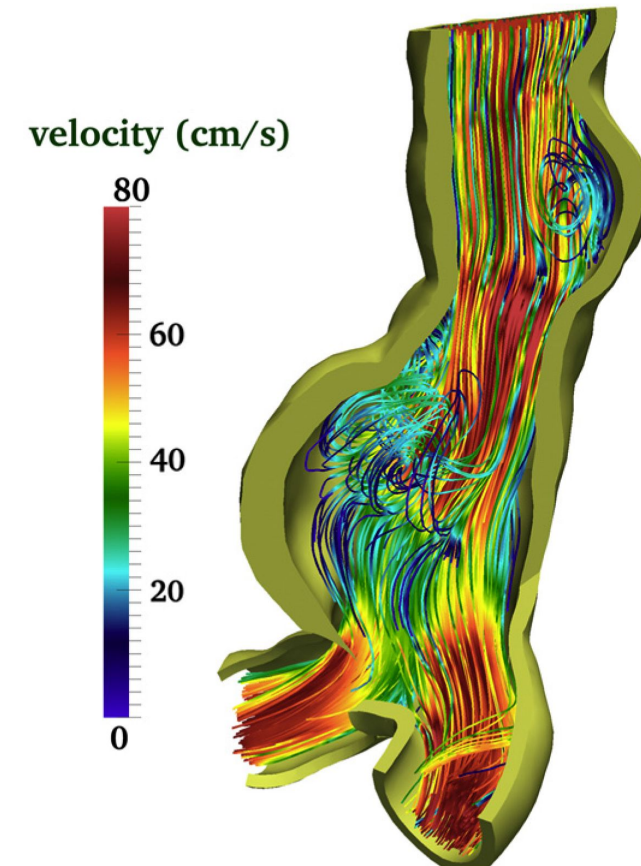


Clot formulation
(illustration from internet)



What for?

- **Three-dimensional** model is needed for decision making in case of complex patient-oriented geometry of blood vessel or arteria.

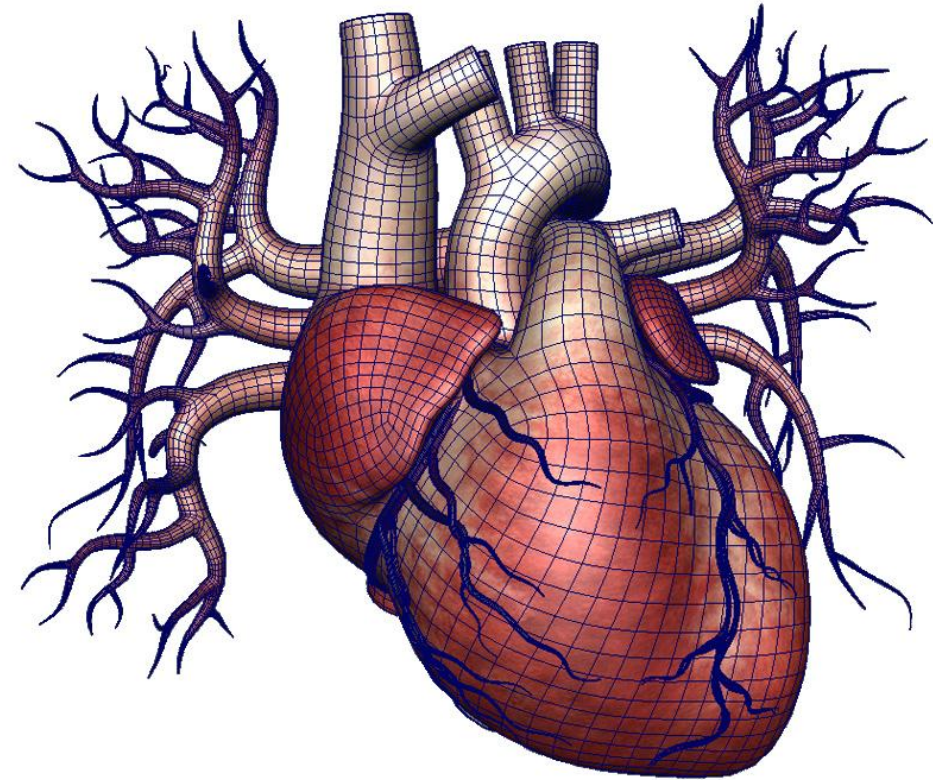


Modeling of aneurysm
(from Quarteroni)



What for?

- Diseases of the heart and blood vessels is the **primary** cause of death
 - thromboembolic complications
- **Three-dimensional** model allows to assess the risk of
 - vessel occlusion
 - myocardial infarction



Heart model



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- The diagram illustrates the blood coagulation cascade. At the top left, Tissue Factor (TF) and Factor VII (FVII) combine to form the active complex TF:FVIIa. This complex activates Factor IX (FIX) and Factor X (FX) to their active forms, FIXa and FXa, respectively. Factor Xa, in the presence of Factor V (FVa) and Factor VIII (FVIII), activates Factor II (FII) to Factor IIa (FIIa). Factor IIa then activates Factor I (FI) to Factor Ia (FIa), which finally leads to the formation of Fibrin polymer (Fp). The diagram also shows the role of platelets: inactive platelets are activated by thrombin (FIIa) to become active platelets. Active platelets release ADP and Thrombolytic Agent III (ATIII), which in turn activate Factor VIII (FVIII) to FVIIIa. FVIIIa then activates Factor IX (FIX) to FIXa, completing the feedback loop. The diagram uses various symbols: a large blue circle for the blood vessel, a blue star for active platelets, and a blue oval for inactive platelets. Arrows indicate the direction of activation, while T-bars indicate inhibition.

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Assumptions

- Blood is considered as an **incompressible Newton's** fluid: no account for **complex nonlinear rheology** of blood
- Blood vessels/arteria are **rigid**: no account for **wall motion**
- Fibrin-polymer is **immobile**: no account for clot **detachment**



System of Equations

- Conservation of momentum:
$$\frac{\partial \rho \mathbf{u}}{\partial t} + \operatorname{div}(\rho \mathbf{u} \mathbf{u}^T - \mu \nabla \mathbf{u} + pI) = \frac{1}{k(F_p, \phi_c)} \mathbf{u}$$
- Incompressibility:
$$\operatorname{div}(\mathbf{u}) = 0$$
- Prothrombin:
$$\frac{\partial P}{\partial t} + \operatorname{div}(P \mathbf{u} - D \nabla P) = -(k_1 \phi_c + k_2 B_a + k_3 T + k_4 T^2 + k_5 T^3) P$$
- Thrombin:
$$\frac{\partial T}{\partial t} + \operatorname{div}(T \mathbf{u} - D \nabla T) = (k_1 \phi_c + k_2 B_a + k_3 T + k_4 T^2 + k_5 T^3) P - k_6 A T$$
- Clot formation factors
FIXa, Fxa:
$$\frac{\partial B_a}{\partial t} + \operatorname{div}(B_a \mathbf{u} - D \nabla B_a) = (k_7 \phi_c + k_8 T)(B^0 - B_a) - k_9 A B_a$$
- Antithrombin:
$$\frac{\partial A}{\partial t} + \operatorname{div}(A \mathbf{u} - D \nabla A) = -k_6 A - k_9 A B_a$$
- Fibrinogen:
$$\frac{\partial F_g}{\partial t} + \operatorname{div}(F_g \mathbf{u} - D \nabla F_g) = -\frac{k_{10} T F_g}{K_{10} + F_g}$$



System of Equations

- Fibrin:
$$\frac{\partial F}{\partial t} + \operatorname{div}(F\mathbf{u} - D\nabla F) = \frac{k_{10}TF_g}{K_{10} + F_g} - k_{11}F$$
- Fibrin-polymer:
$$\frac{\partial F_p}{\partial t} = k_{11}F$$
- Inactivated platelets:
$$\frac{\partial \phi_c}{\partial t} + \operatorname{div}\left(\tanh\left(\pi\left(1 - \frac{\phi_c + \phi_f}{\phi_{\max}}\right)\right)(\phi_c\mathbf{u} - D_p\nabla\phi_c)\right) = -(k_{12}T - k_{13}\phi_c)\phi_f$$
- Activated platelets:
$$\frac{\partial \phi_f}{\partial t} + \operatorname{div}\left(\tanh\left(\pi\left(1 - \frac{\phi_c + \phi_f}{\phi_{\max}}\right)\right)(\phi_f\mathbf{u} - D_p\nabla\phi_f)\right) = (k_{12}T - k_{13}\phi_c)\phi_f$$
- Media permeability:
$$\frac{1}{k(F_p, \phi_c)} = \frac{16}{a^2} \tilde{F}_p^{\frac{3}{2}} (1 + 56\tilde{F}_p) \frac{\phi_{\max} + \phi_c}{\phi_{\max} - \phi_c} \quad \text{with} \quad \tilde{F}_p = \min\left(\frac{7}{10}, \frac{F_p}{7000}\right)$$

Bouchnita, A., Terekhov, K., Nony, P., Vassilevski, Y., & Volpert, V.: **A mathematical model to quantify the effects of platelet count, shear rate, and injury size on the initiation of blood coagulation under venous flow conditions.** PloS one, 15(7), e0235392, 2020



Boundary Conditions

- BC on blood vessel damage:

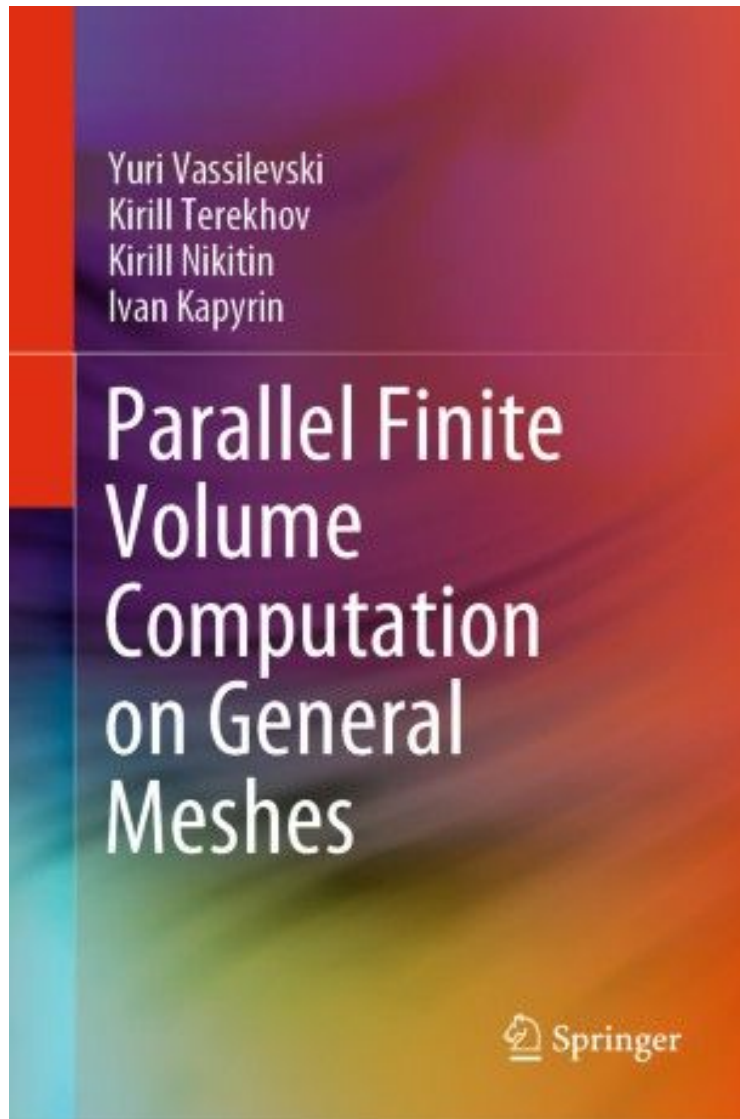
$$\frac{\partial B_a}{\partial \mathbf{n}} = \frac{\alpha(B^0 - B_a)}{1 + \beta(B^0 - B_a)}$$

- BC for Navier-Stokes:
 - no-slip condition on walls
 - pressure drop between inflow and outflow
- BC of Dirichlet/Neumann type for blood components
- Model parameters:
 - from literature,
 - from 0D thrombin generation model,
 - tuned.



Numerical Methods

for model construction



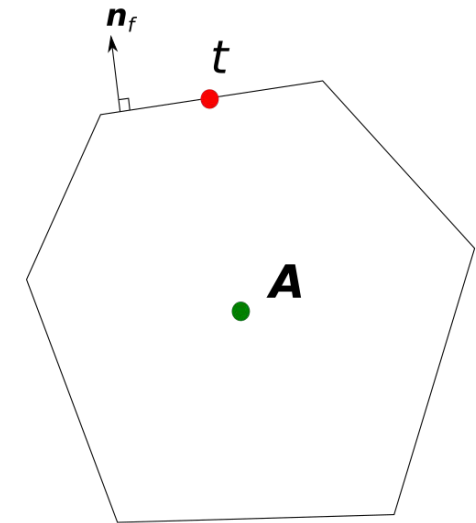
- Vassilevski, Y., Terekhov, K., Nikitin, K., & Kapyrin, I. (2020). **Parallel Finite Volume Computation on General Meshes**. Springer Nature.
- Terekhov, K. (2020). **Collocated Finite-Volume Method for the Incompressible Navier-Stokes Problem**. Journal of Numerical Mathematics



Finite-Volume Method

- Ostrogradsky-Gauss theorem:

$$\begin{aligned} -\operatorname{div}(\mathbf{A}) = g &\implies - \oint_{\partial V} \mathbf{A} d\mathbf{S} = \int_V g dV \\ &\implies - \sum_{f \in \mathcal{F}(V)} |f| \mathbf{A} \mathbf{n}|_{\mathbf{x}_f} = |V| g|_{\mathbf{x}_V} \end{aligned}$$



- Requires the **flux approximation**:

$$t = \mathbf{A} \mathbf{n}|_{\mathbf{x}_f}$$



FVM for Navier-Stokes

- Full flux expression:

$$t = \left\{ \begin{array}{l} \rho \mathbf{u} \mathbf{u}^T \mathbf{n} - \mu \nabla \mathbf{u} \mathbf{n} + p \mathbf{n} \\ n^T \mathbf{u} \end{array} \right|_{\mathbf{x}_f}$$

- Second-order** Taylor Series approximation:

$$\rho \mathbf{u} \mathbf{u}^T \mathbf{n} \big|_{\mathbf{x}_f} \approx \rho \mathbf{u} \mathbf{u}^T \mathbf{n} \big|_{\mathbf{x}_1} + \rho \frac{\partial \mathbf{u} \mathbf{u}^T \mathbf{n}}{\partial \mathbf{u}} \bigg|_{\mathbf{x}_1} \nabla \mathbf{u} (\mathbf{x}_f - \mathbf{x}_1)$$

- Upstream** approximation:

$$\rho \mathbf{u} \mathbf{u}^T \mathbf{n} \big|_{\mathbf{x}_f} \approx \frac{\rho}{2} \left(\mathbf{u}_1 \mathbf{n}^T + \mathbf{n}^T \mathbf{u}_1 \mathbb{I} \right) \times \begin{cases} 3\mathbf{u}_1 - 2\mathbf{u}_f + 4\nabla \mathbf{u}(\mathbf{x}_f - \mathbf{x}_1), & \mathbf{n}^T \mathbf{u}_1 > 0, \\ 2\mathbf{u}_f - \mathbf{u}_1, & \mathbf{n}^T \mathbf{u}_1 < 0. \end{cases}$$

3x3 matrix $Q(\mathbf{u}_1)$, eigenvalues $\mathbf{n}^T \mathbf{u}_1, 2\mathbf{n}^T \mathbf{u}_1, 0$



FVM for Navier-Stokes

- Full flux expression:

$$t = \left\{ \begin{array}{c} \rho u u^T n - \mu \nabla u n + p n \\ n^T u \end{array} \right|_{\mathbf{x}_f}$$

- **Second-order** splitting:

$$-\mu \nabla u n|_{\mathbf{x}_f} \approx \underbrace{\mu (u_1 - u_f) / r_1}_{\text{Two-point part}} - \underbrace{\mu \nabla u (n - (\mathbf{x}_f - \mathbf{x}_1) / r_1)}_{\text{Transversal correction}}$$

Distance to interface

- Two-point yields positive matrix coefficients.
- Transversal correction is zero on orthogonal grids.



FVM for Navier-Stokes

- Full flux expression:

$$t = \left\{ \begin{array}{c} \rho u u^T n - \mu \nabla u n + p n \\ n^T u \end{array} \right\} \bigg|_{\mathbf{x}_f}$$

- Stable** approximation:

$$\begin{aligned} \left\{ \begin{array}{c} p n \\ n^T u \end{array} \right\} &= \begin{bmatrix} n^T & n \end{bmatrix} \begin{bmatrix} u \\ p \end{bmatrix} \\ &\approx \begin{bmatrix} \xi n n^T & n \\ 0^T & n \end{bmatrix} \begin{bmatrix} u_1 \\ p_1 \end{bmatrix} + \begin{bmatrix} -\xi n n^T & 0 \\ n^T & 0 \end{bmatrix} \begin{bmatrix} u_f \\ p_f \end{bmatrix} \\ &+ \begin{bmatrix} \xi n n^T & 0 \end{bmatrix} \begin{bmatrix} \nabla u (\mathbf{x}_f - \mathbf{x}_1) \end{bmatrix} \end{aligned}$$

Positive and negative eigenvalues

Positive eigenvalues

Negative eigenvalues

Compensation term



FVM for Navier-Stokes

- Full flux expression:

$$\mathbf{t} = \left\{ \begin{array}{c} \rho \mathbf{u} \mathbf{u}^T \mathbf{n} - \mu \nabla \mathbf{u} \mathbf{n} + p \mathbf{n} \\ \mathbf{n}^T \mathbf{u} \end{array} \right\} \Big|_{\mathbf{x}_f}$$

- Combination of approximations:

$$\begin{aligned} \mathbf{t} \approx & \left(\frac{3}{2} Q(\mathbf{u}_1)^+ - \frac{1}{2} Q(\mathbf{u}_1)^- + \frac{\mu}{r_1} \mathbb{I} + \xi \mathbf{n} \mathbf{n}^T \right) \mathbf{u}_1 \\ & - \left(Q(\mathbf{u}_1)^+ - Q(\mathbf{u}_1)^- + \frac{\mu}{r_1} \mathbb{I} + \xi \mathbf{n} \mathbf{n}^T \right) \mathbf{u}_f \\ & - \nabla \mathbf{u} \left(\mu \mathbf{n} - \left(\frac{\mu}{r_1} \mathbb{I} + \xi \mathbf{n} \mathbf{n}^T + 2Q(\mathbf{u}_1)^+ \right) (\mathbf{x}_f - \mathbf{x}_1) + p_1 \mathbf{n} \right) \end{aligned}$$

- Interface unknown elimination is based on the flux continuity.
- Computation of gradients is based on Green's formula



FVM for Blood Components

- Flux expression: $\mathbf{n}^T(C\mathbf{u} - D\nabla C)$
- Advection: **first-order** upstream:

$$C\mathbf{n}^T\mathbf{u} \approx \frac{1}{2} (C_1(\mathbf{n}^T\mathbf{u} + |\mathbf{n}^T\mathbf{u}|) + C_2(\mathbf{n}^T\mathbf{u} - |\mathbf{n}^T\mathbf{u}|))$$

- Diffusion: **second-order** nonlinear two-point approximation:

- $$D\mathbf{n}^T\nabla C \approx D \frac{(C_1 - C_2)}{|\mathbf{x}_1 - \mathbf{x}_2|} - D(\mu_1\nabla C_1 + \mu_2\nabla C_2) \cdot \left(\mathbf{n} - \frac{(\mathbf{x}_1 - \mathbf{x}_2)}{|\mathbf{x}_1 - \mathbf{x}_2|} \right) = D(T_1C_1 - T_2C_2)$$

- Solution is **nonnegative** – very important for reactions!



FVM for Traffic Flow

- Flux expression: $\lambda(C)\mathbf{n}^T\mathbf{u}$
 - advection: $\lambda(C) = C$
 - traffic: $\lambda(C) = C(1 - C)$
 - our case: $\lambda(C) = C \tanh(1 - C)$
- First-order** upstream approximation:

$\lambda'(C_1)\mathbf{n}^T\mathbf{u}$	$\lambda'(C_1)\mathbf{n}^T\mathbf{u}$	t
+	+	$\lambda(C_1)\mathbf{n}^T\mathbf{u}$
-	-	$\lambda(C_2)\mathbf{n}^T\mathbf{u}$
+	-	$\min(\lambda(C_1), \lambda(C_2))\mathbf{n}^T\mathbf{u}$
-	+	$\lambda(C)\mathbf{n}^T\mathbf{u}, \lambda'(C) = 0$



Moscow traffic
(image from internet)



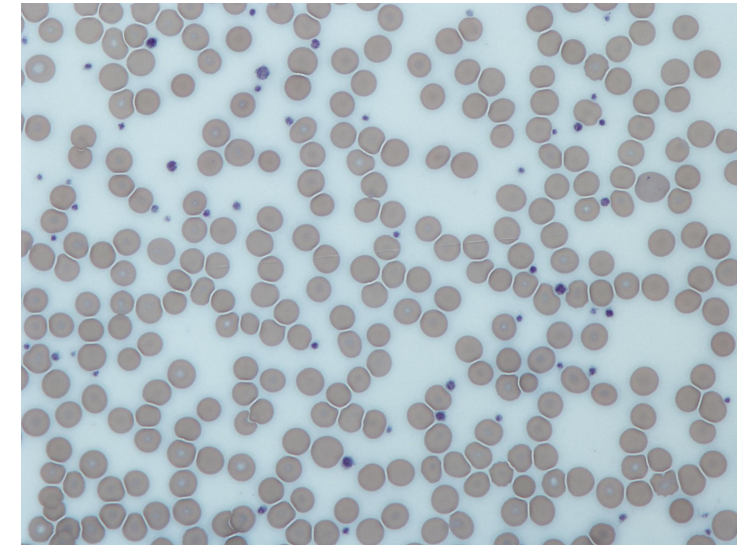
FVM for Platelets

- Flux expression: $t(\phi_c, \phi_f) = \tanh\left(\pi\left(1 - \frac{\phi_c + \phi_f}{\phi_{max}}\right)\right) \mathbf{n}^T (\mathbf{u} - D_p \nabla) \begin{pmatrix} \phi_c \\ \phi_f \end{pmatrix}$
- Jacobian contribution:

$$J(\phi_c, \phi_f) = \begin{pmatrix} \frac{\partial \mathbf{t}_1(\phi_c, \phi_f)}{\partial \phi_c} & \frac{\partial \mathbf{t}_1(\phi_c, \phi_f)}{\partial \phi_f} \\ \frac{\partial \mathbf{t}_2(\phi_c, \phi_f)}{\partial \phi_c} & \frac{\partial \mathbf{t}_2(\phi_c, \phi_f)}{\partial \phi_f} \end{pmatrix} \begin{pmatrix} d\phi_c \\ d\phi_f \end{pmatrix} = Q(\phi_c, \phi_f) \begin{pmatrix} d\phi_c \\ d\phi_f \end{pmatrix}$$

- Matrix-weighted combination for two cells:

$$\Phi = M_1 \begin{pmatrix} \phi_{c,1} \\ \phi_{f,1} \end{pmatrix} + M_2 \begin{pmatrix} \phi_{c,2} \\ \phi_{f,2} \end{pmatrix}$$



Platelets
(image from internet)



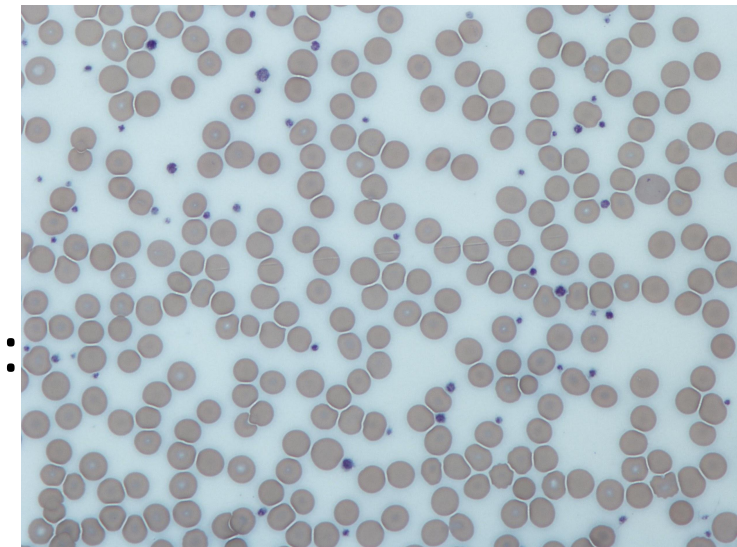
FVM for Platelets

- Flux expression: $t(\phi_c, \phi_f) = \tanh\left(\pi\left(1 - \frac{\phi_c + \phi_f}{\phi_{max}}\right)\right) \mathbf{n}^T (\mathbf{u} - D_p \nabla) \begin{pmatrix} \phi_c \\ \phi_f \end{pmatrix}$
- Iterative search:

$$J(\Phi) = Q(\Phi)M_1 \begin{pmatrix} d\phi_{c,1} \\ d\phi_{f,1} \end{pmatrix} + Q(\Phi)M_2 \begin{pmatrix} d\phi_{c,2} \\ d\phi_{f,2} \end{pmatrix}$$

- Matrices are obtained using eigendecomposition:

$$\begin{aligned} Q(\Phi) &= L\Lambda L^T, \\ M_1 &= \frac{1}{2}L(\text{sgn}(\Lambda) + |\text{sgn}(\Lambda)|)L^T \\ M_2 &= \frac{1}{2}L(\text{sgn}(\Lambda) - |\text{sgn}(\Lambda)|)L^T \end{aligned}$$



Platelets
(image from internet)



Approximation for Reactions

- Reactions lead to very **small time step** even with fully implicit integration.
- Problem – **bad contribution** to off-diagonal terms of Jacobian matrix.
- Approach for terms leading to bad contribution:
 - time extrapolation, **physics-based limiter for extrapolation**
 - space interpolation



Approximation for Reactions

- Red terms are extrapolated from previous time steps:

$$R(\Theta^{n+1}) \approx \begin{pmatrix} -\left(k_1 \hat{\phi}_c + k_2 B_\alpha^{n+1} + k_3 \hat{T} + k_4 \hat{T}^2 + k_5 \hat{T}^3\right) P^{n+1} \\ \left(k_1 \hat{\phi}_c + k_2 B_\alpha^{n+1} + k_3 \hat{T} + k_4 \hat{T}^2 + k_5 \hat{T}^3\right) P - k_6 A^{n+1} T^{n+1} \\ \left(k_7 \phi_c^{n+1} + k_8 T^{n+1}\right) \left(B^0 - B_\alpha^{n+1}\right) - k_9 A^{n+1} B_\alpha^{n+1} \\ - \left(k_6 T^{n+1} + k_9 B_\alpha^{n+1}\right) A^{n+1} \\ - \frac{k_{10} \hat{T} F_g^{n+1}}{K_{10} + F_g^{n+1}} \\ \frac{k_{10} \hat{T} F_g^{n+1}}{K_{10} + F_g^{n+1}} - k_{11} F^{n+1} \\ k_{11} F^{n+1} \\ - \left(k_{12} \hat{T} - k_{13} \phi_c^{n+1}\right) \phi_f^{n+1} \\ \left(k_{12} \hat{T} - k_{13} \phi_c^{n+1}\right) \phi_f^{n+1} \end{pmatrix} \begin{matrix} P \\ T \\ B \\ A \\ \cancel{A} \\ F \\ \cancel{F} \\ F \\ \phi_f \\ \phi \\ c \end{matrix}$$

- Fully implicit model with 13 unknowns.



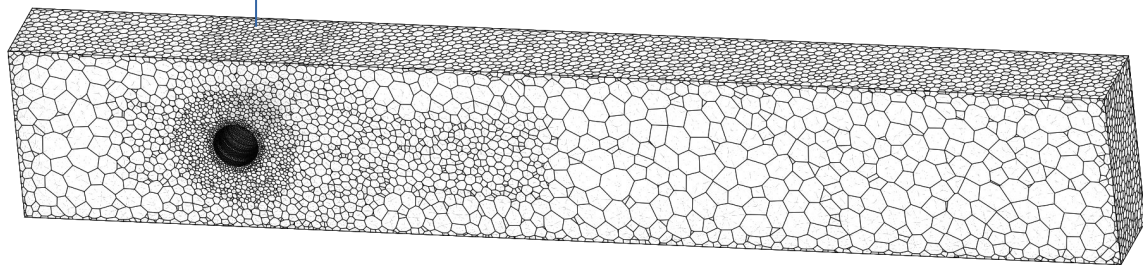
Verification

of the model

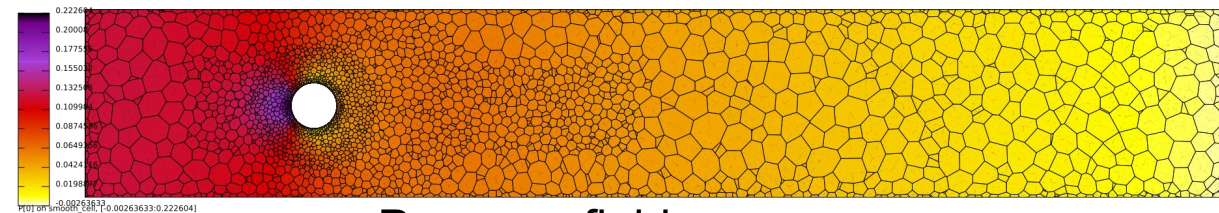


Viscous Flow Past a Cylinder

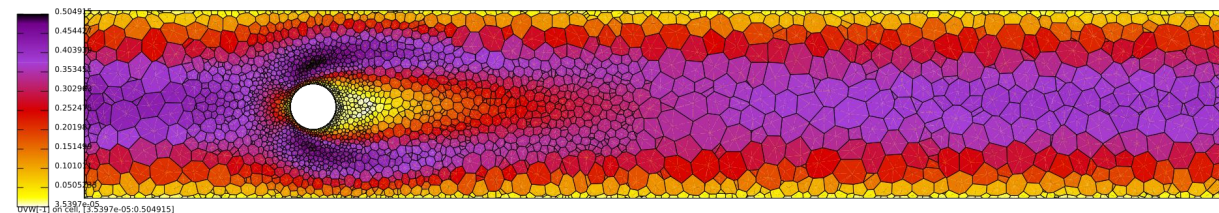
Refinement	Cells	Drag	Lift	Pressure drop
1	910	3.862	-0.08556	0.1481
2	4328	4.964	-0.02525	0.1854
3	24687	5.515	0.07256	0.1672
4	164806	5.876	0.00803	0.1890
3 [†]	53211	6.064	0.01015	0.1801
3 [‡]	98517	6.155	0.01006	0.1792
Schäfer & Turek [23]	-	6.05-6.25	0.008-0.01	0.165-0.175
Braack & Richter [7]	-	<u>6.185331</u>	<u>0.00940</u>	<u>0.1713</u>



Locally refined polyhedral mesh



Pressure field

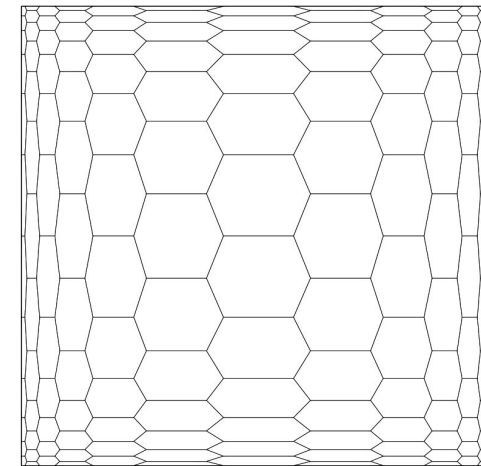
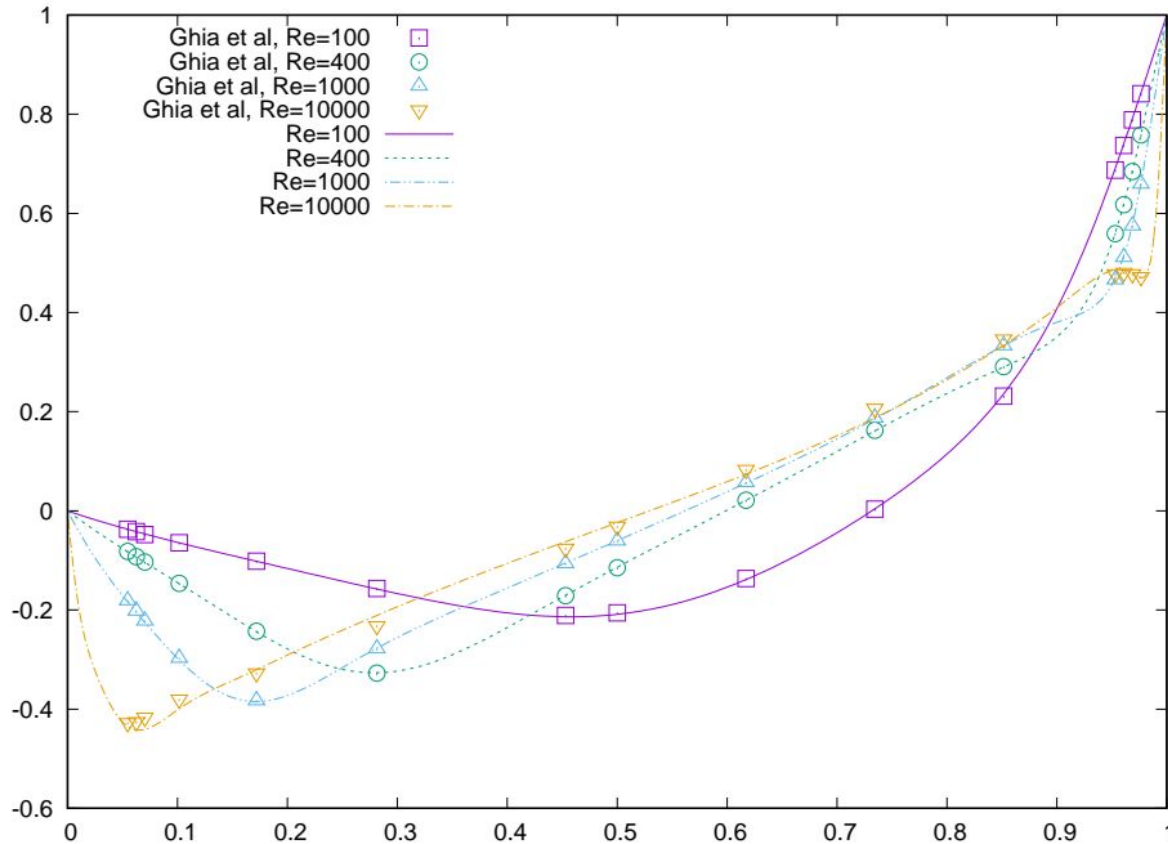


Velocity magnetude

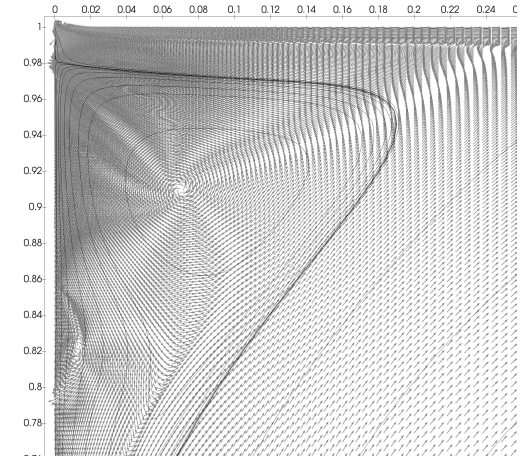


Cavity Flow at High Reynolds Numbers

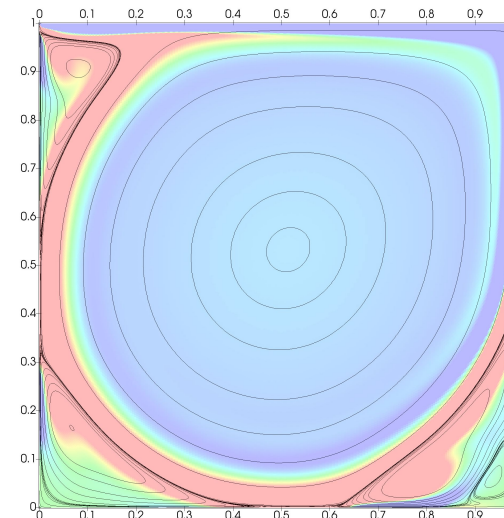
- Comparison to reference data of Ghia et al.



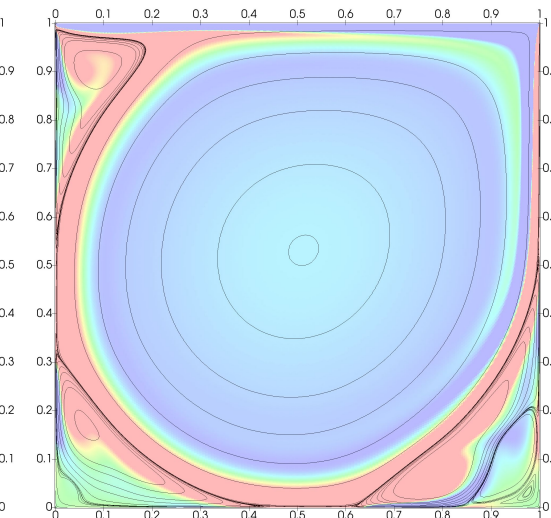
Hexagonal mesh



Tertiary vortex, Re = 16000



Re = 10000

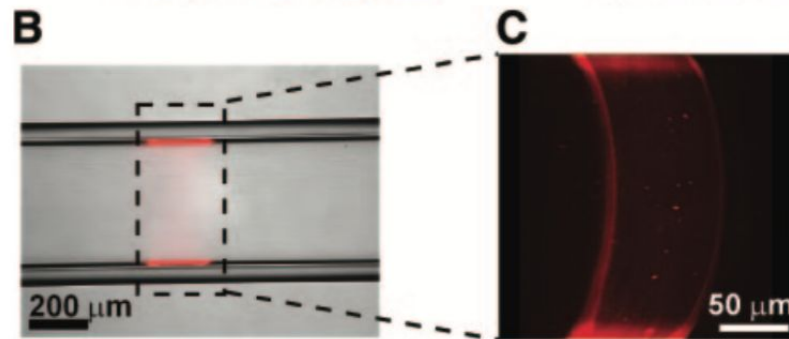
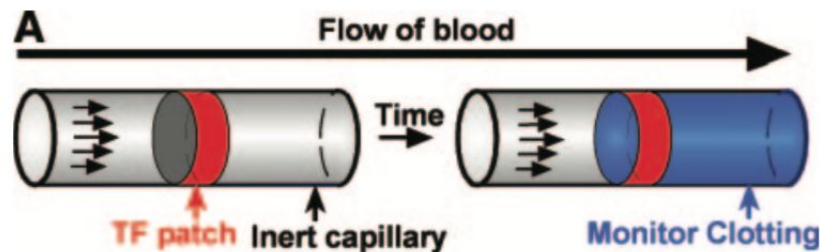


Re = 16000

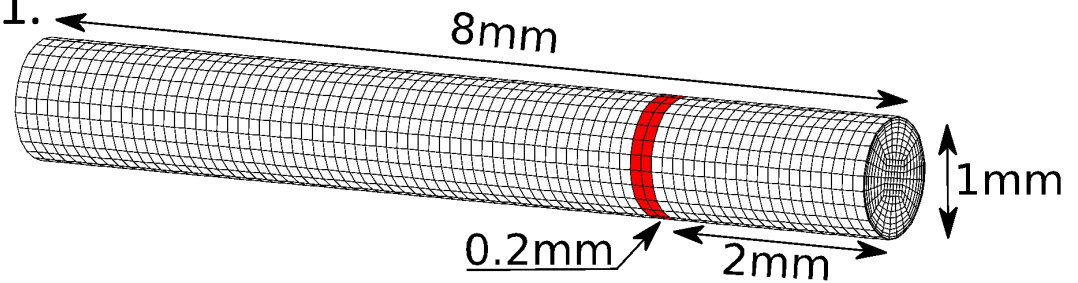


Comparison to the Experimental Data

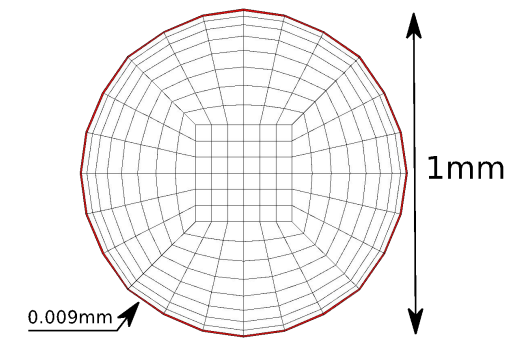
- Based on the **experimental research**: Shen F., Kastrup C.J., Liu Y., Ismagilov R.F.: *Threshold response of initiation of blood coagulation by tissue factor in patterned microfluidic capillaries is controlled by shear rate. Arteriosclerosis, thrombosis, and vascular biology.* 2008, 28(11): 2035–2041.



Experiment illustration



Computational domain

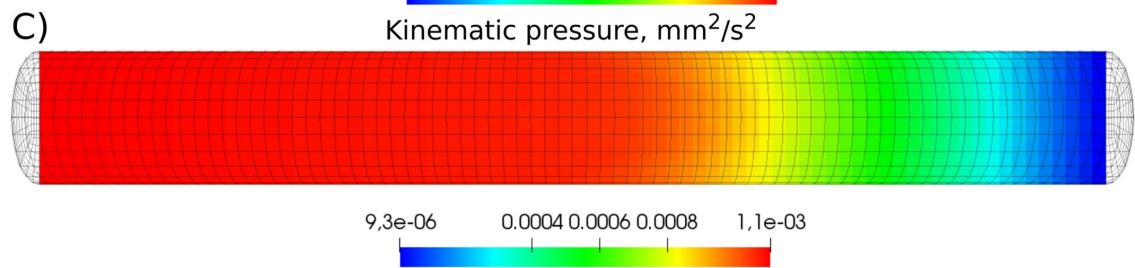
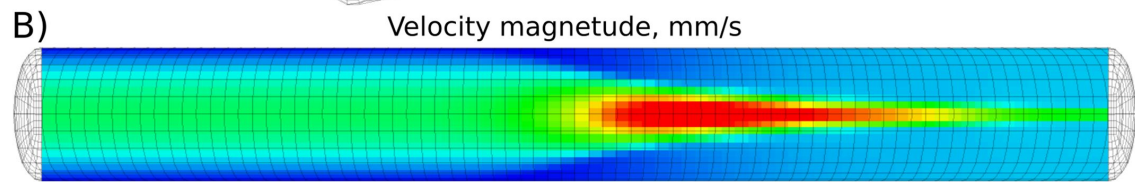
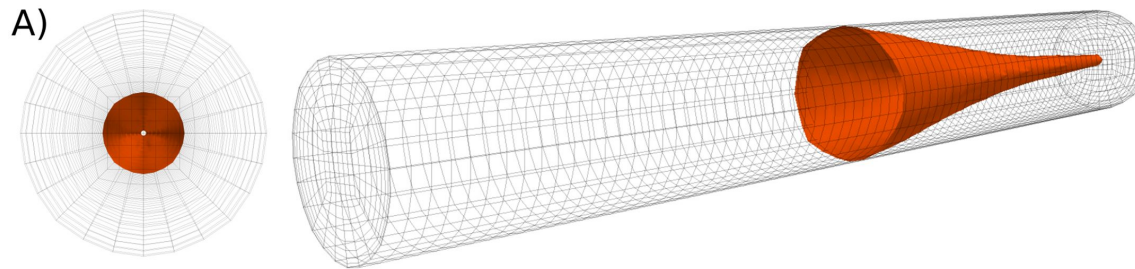


Section of the cylinder

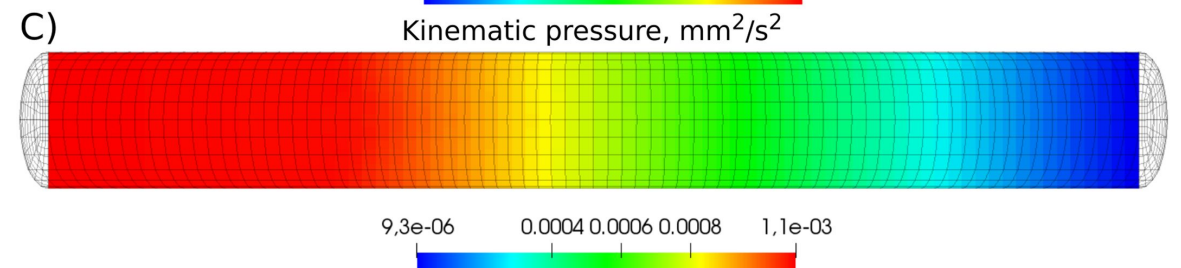
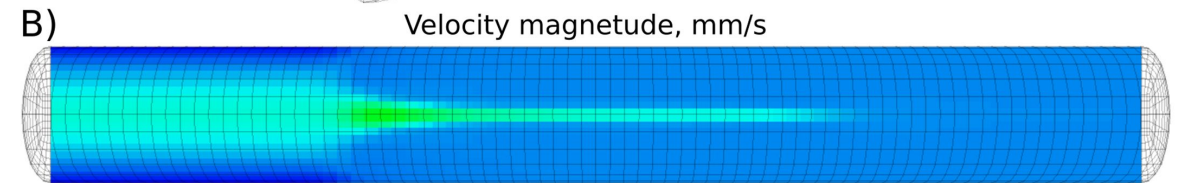
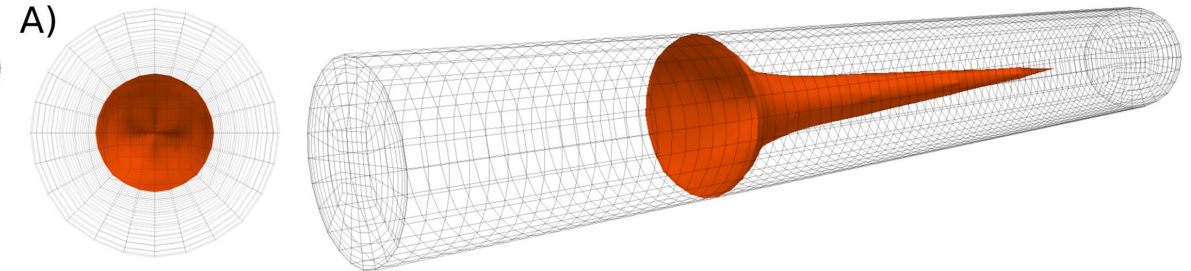


Comparison to the Experimental Data

T=60s



T=70s

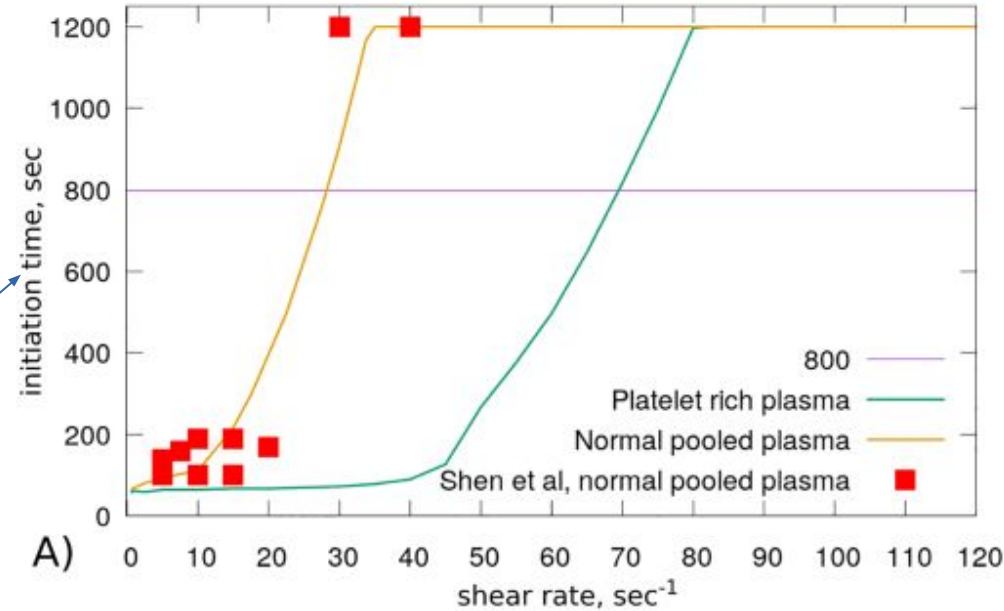


Reproduction of qualitative characteristics of the experiment

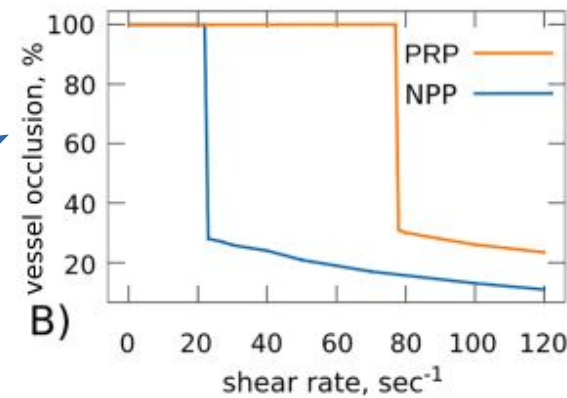


Comparison to the Experimental Data

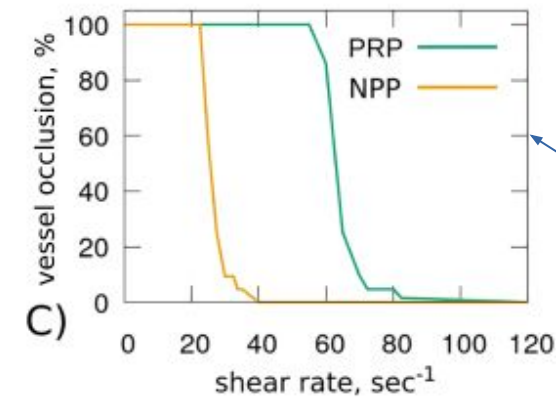
A) Validation of 3D model on experimental data



B) Simplified 1D clot formation model



C) Full 3D simulation of clot formation

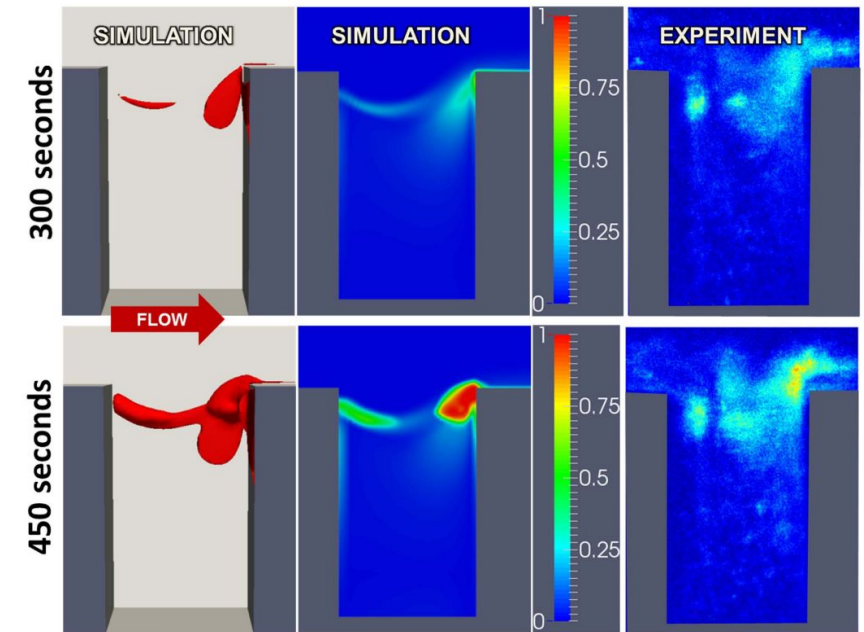
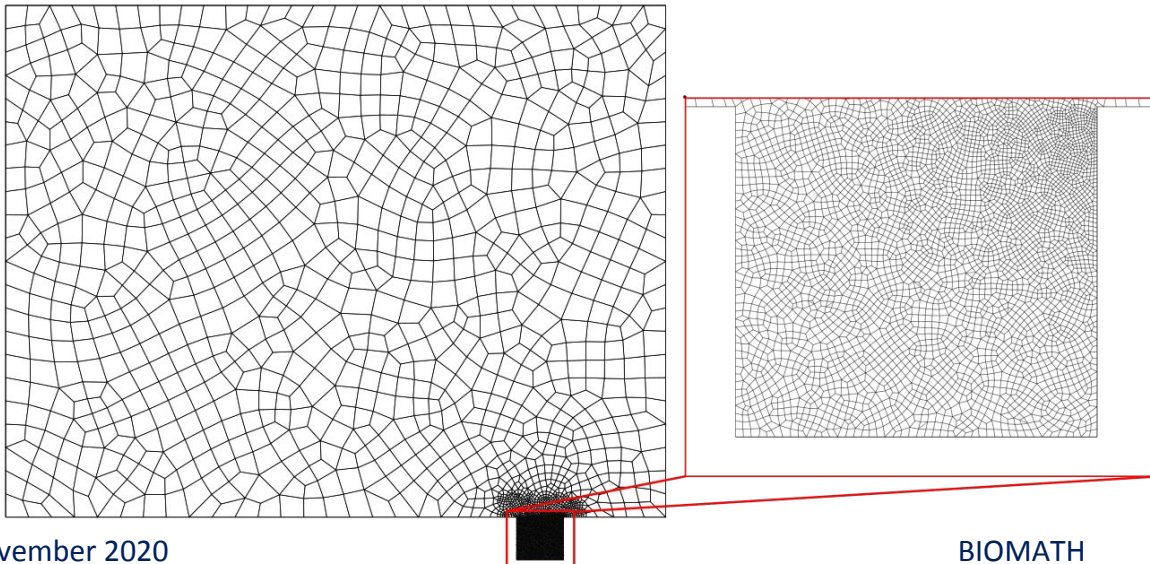


Bouchnita, A., Terekhov, K., Nony, P., Vassilevski, Y., & Volpert, V.: **A mathematical model to quantify the effects of platelet count, shear rate, and injury size on the initiation of blood coagulation under venous flow conditions.** PloS one, 15(7), e0235392, 2020



Future Directions

- Clot formation due to von Willebrand factor in the flow with high shear rate (Nadezhda Suslova)
- Automatic stabilization of chemical reactions (Ivan Butakov)



from Wei-Tai Wu et al,
Multi-Constituent Simulation
Of Thrombus Deposition

Thank you for your attention!

Contacts

- KIRILL.TEREHOV@GMAIL.COM
- YURI.VASSILEVSKI@GMAIL.COM

Links

- WWW.INMOST.ORG

